

BACKGROUND OF THE INVENTION

Field of the Invention

The present invention relates to surface coverings, particularly surface coverings having a natural appearance. The present invention further relates to methods of making these types of surface coverings.

Description of the Related Art

A growing consumer preference for natural materials or "looks" simulated to natural wood, stone, marble, brick, and granite now exists for all types of surface coverings such as flooring. The perception of natural flooring, for instance, at an inexpensive price provides a high value, acceptable style, and luxury appearance.

The natural look of resilient vinyl floorings, for instance, made by gravure printing in conjunction with chemical embossing technology, does not quite impart the realistic appearance of true wood, stone, and the like. The subtle texture of wood grains and stone cannot be achieved by chemical embossing technology which develops the texture by reacting the inhibitor in the ink with a blow agent added in a pre-gel layer under heat and during a fusion process. In general, the texture created by the chemical embossing technique does not have a well-defined sharpness of real, natural products. In other words, chemical embossing has the disadvantage of being capable of making only rounded edges and there is great difficulty in controlling the depth of the embossing. In addition, this process leads to a texture which is too deep to be realistic. Mechanical embossing, on the other hand, is capable of reproducing the subtle, sharp,

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BRIEF DESCRIPTION OF THE DRAWINGS

This invention will be described in greater detail with reference to the drawings in which:

FIG. 1 depicts a side view of the apparatus for embossing the surface covering of the present invention.

FIG. 2 is a fragmentary, cross-sectional view of the surface covering of the present invention depicting the multiple layers in detail.

FIG. 3 is a microscope photograph of the surface covering of the present invention.

DETAILED DESCRIPTION OF THE PRESENT INVENTION

Generally, a surface covering can be made by the present invention which combines chemical embossing with mechanical embossing to form a unique product. Preferably, this product is a surface covering having a natural wood, stone, marble, granite, or brick appearance, though other surface coverings having the desired combination of chemical embossing and mechanical embossing as described herein form part of the present invention. For purposes of the present invention, surface covering includes, but is not limited to, flooring such as inlaid floors, hardwood floors, solid vinyl tiles, homogeneous floors, cushioned floors, and the like; wall paper; laminates; and countertops.

In making the surface covering, a backing layer or substrate A is provided and a foamable layer C and D is formed or placed on top of backing layer A as shown in FIG. 2. A design or print layer B is applied, adhered, or located on top of the foamable layer as seen in FIG. 2. The design layer B has a design (not

shown) and a portion of this design is formed with a retarder composition, such as, but not limited to, a retarder ink. Preferably, the portion of the design is in the shape and form of one or more joint or grout lines (not shown) which simulate, for instance, the joint lines between two strips of wood forming a surface covering or the joining of stones, marble, granite, or brick by mortar or grout lines between each stone, marble, granite, or brick.

Once the design layer B is applied, a wear layer is applied or located on top of the design layer and the surface covering, and the wear layer is then cured such as by subjecting the surface covering to heat to form a cured wear layer.

This curing process will also chemically emboss areas of the design layer where the retarder ink has been applied. In the preferred embodiment, the chemically embossed areas are the printed joint or grout lines. Any heating means can be used, such as a gas-fired forced-hot-air oven. The product is then permitted to obtain ambient temperature, such as by cooling. Afterwards, the surface of the product is subjected to a sufficient temperature to soften the cured wear layer surface, for instance, through re-heating, preferably by infrared radiant heat.

This softens the surface in order to enable the product to receive the mechanical embossing. The wear layer is then mechanically embossed to have a surface texture. Any surface texture can be embossed onto the wear layer. Preferably, the surface texture simulates or has a wood, stone, marble, granite, or brick surface texture. During mechanical embossing, the foam layer may or may not be mechanically embossed. It is preferred that the foam layer is slightly

embossed. In particular, in a preferred embodiment, the portions of the wear

layer being mechanically embossed will compress or lose from about 1 to about 4 mils in thickness while the portions of the foam layer in contact with these portions will compress or lose from about 1 to about 5 mils in thickness. In this preferred embodiment, the total embossing depth of wear layer and foam layer combined is between about 3 mils and about 8 mils. Preferably, the foam cells within the foam layer are not crushed or collapsed in the embossed areas, but may be flattened or distorted as shown in D in FIG. 2.

A top coat (not shown in FIG. 2) may then be provided on top of the embossed wear layer to form the surface covering.

The backing layer used in the present invention can be any conventional backing layer used in surface coverings such as a felted or matted fibrous sheet of overlapping, intertwined filaments and/or fibers, usually of natural, synthetic, or man-made cellulosic origin, such as cotton or rayon, although many other forms of sheets, films, textile materials, fabrics, or the like, may be used. The substrate or backing layer can be non-foamed, non-crosslinked vinyl compositions as well. The thickness of a conventional substrate layer is generally not critical and it is preferably from about 2 to about 100 mils, more preferably from about 15 to about 30 mils.

The foamable layer used in the present invention can be any conventional foamable layer used in surface coverings, such as a foam layer used in flooring. In particular, the foamable layer can be any suitable material known in the art for producing foam layers such as polyvinyl chloride plastisol or organosol.

Alternatively, and preferably, the foam layer is a resilient, cellular foam layer which can be formed from a resinous composition containing a foaming or blowing agent that causes the composition to expand on heating. It is also known in the art that foamable, resinous sheet material can be selectively embossed by controlling the decomposition temperature of a catalyzed blowing or foaming agent in the heat-expandable composition. For example, by applying to the heat-expandable composition a reactive chemical compound which is referred to in the art as a "regulator," "inhibitor," or "retarder," it is possible to modify the decomposition temperature of the catalyzed foaming or blowing agent in the area of application of the reactive compound. It is thus possible to produce sheet materials having surface areas that are depressed with inhibitor application and raised proximate the area without inhibitor application.

The inhibitor or retarder can be conveniently incorporated in an inhibitor or retarder composition, preferably in a foam-retarding, printing ink composition, which is printed over the heat-expandable resinous composition. Such compositions are well-known in the art and are generally based on an organic solvent carrier or vehicle system. Alternatively, and preferably, an aqueous retarder printing ink composition is used such as the one described in U.S. Patent No. 5,169,435, incorporated in its entirety by reference herein. A most preferred aqueous retarder printing ink composition contains from about 20 to about 30% by weight acrylic resin binder, from about 6.5 to about 17% by weight tolyltriazole, from about 20 to about 30% by weight alcohol, and from about 35 to about 50% by weight water. Foaming or blowing agent modifiers or inhibitors

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and include, but are not limited to, a reverse-roll coater. Once the wear layer is applied to the top of the foamable layer, the wear layer is cured. This curing can be accomplished by subjecting the wear layer along with the foamable layer and substrate to a sufficient temperature, e.g., by heating, to cure the wear layer in a multi-zone gas-fired hot air oven essentially as described in U.S. Patent No. 3,293,108. Also, the curing or heating step will expand the foamable layer to form the foam layer which will have chemically embossed areas. For purposes of curing the wear layer, a sufficient temperature for a sufficient time would be used and known to those skilled in the art. Preferably, this temperature is from about 195°C to about 215°C for a time of from about 2.0 minutes to about 3.0 minutes, more preferably about 2.0 minutes to about 2.2 minutes.

Once the wear layer is cured, it is preferred to permit the wear layer to obtain an ambient temperature, such as by passing it over a series of water-cooled drums or "cans" essentially as described in U.S. Patent No. 3,293,108. The wear layer is then subjected to a sufficient temperature for a sufficient time in order to soften the wear layer to a sufficient degree to allow it to be mechanically embossed. The surface temperature of the wear layer for purposes of mechanically embossing it is preferably from about 145°C to about 160°C depending on, among other things, the color of the printed design under the wear layer surface. The mechanical embossing of the wear layer can be achieved in such a manner that the foam layer beneath the wear layer may or may not be mechanically embossed. In any event, the portion of the the foam layer which has been overlayed with the design layer having the retarder

Figure 1 illustrates the steps of the proposed algorithm for finding a minimum spanning tree. The process starts with a graph with 10 nodes and 15 edges. The algorithm iteratively selects edges with the lowest weight that do not create a cycle or result in a vertex with a degree greater than 2. The steps are as follows:

- (a) Initial graph with 10 nodes and 15 edges.
- (b) Select edge (1,2) with weight 1.
- (c) Select edge (2,3) with weight 2.
- (d) Select edge (3,4) with weight 3.
- (e) Select edge (4,5) with weight 4.
- (f) Select edge (5,6) with weight 5.
- (g) Select edge (6,7) with weight 6.
- (h) Select edge (7,8) with weight 7.
- (i) Select edge (8,9) with weight 8.
- (j) Select edge (9,10) with weight 9.
- (k) Select edge (1,10) with weight 10.
- (l) Final minimum spanning tree with 9 edges and total weight 45.

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process, which does not create the mechanically embossed surface texture in the joint or grout lines, imparts to the surface covering the appearance of mechanical embossing in register.

It is certainly within the bounds of the present invention to use several devices to mechanically emboss different textures onto the wear layer. In the preferred embodiment of the present invention, the device used to mechanically emboss will have a pattern that will simulate the surface texture of wood, stone, marble, granite, or brick and this texture will be transferred onto the wear layer.

In accordance with the invention and as shown in FIG. 1, a cured, foamed and cooled surface covering is processed as follows to produce a surface having a "natural" appearance. A web of cooled cushioned covering is passed through the "WEB GUIDE" at the point indicated by the entry arrow. This "WEB GUIDE" is provided to insure that the web tracks straight through the embosser nip. After exiting the "WEB GUIDE", the web passes under the five burners of the "IR HEATER". The heat output of the "IR HEATER" is adjusted as necessary to properly heat the surface of the web by adjusting the height of the burners above the web, and by adjusting the gas flow to the burners. From the "IR HEATER" the web proceeds to the "EMBOSSER". The hot surface of the web contacts an engraved steel embossing roll. The embossing nip, mentioned above, consists of this engraved steel embossing roll and a rubber bed roll, which contacts the back surface of the web. The rubber bed roll is provided with a steel back-up roll which can be used, if necessary, to counteract any tendency of the rubber roll to "bow" downward. The web is maintained in contact with the water-cooled

embossing roll for about 90 degrees of wrap by means of the uppermost idler roll. This contact with the cooled embossing roll surface removes some of the heat from the surface of the web by heat transfer from the web sheet to the water-cooled steel embossing roll, and thus "sets" the embossing. The dwell time is dependent on exact embossing roll circumference and line speed and can be easily determined by one skilled in the art. Approximate dwell time ranges are given for three possible web speeds in Table I below.

TABLE I

Web Speed (ft./min.)	Dwell Time Range (seconds)
48	1.6-1.8
60	1.3-1.4
70	1.1-1.2

The cooled embossed web is then directed back under the "IR HEATER" section of the apparatus. At the point indicated by the exit arrow, the web continues on to a final coating station (not shown) for applying a top-coat to the surface of the web as described below. The apparatus for this coating station is well known to those skilled in the art.

As indicated above, a critical feature of the invention is the surface temperature of the web at the exact instant when the web sheet enters the embossing roll nip. This temperature is dependent on the thickness of the layer, the speed of the moving web, and the exact position where the measurement is taken. However, this exact spot is not generally accessible for temperature

measurements because of the diameter of the embossing roll. Normally, therefore, the reading is taken from the mid-point of the distance between the end of the IR heater and the embossing roll nip. The actual temperature as the web sheet enters the embossing roll nip will be lower than this reading because of heat loss from the web sheet surface as it moves through the space between the measurement point and the embossing roll nip. The faster the line speed, the less opportunity for heat loss and the closer the actual temperature will be to the measured temperature at the embossing nip.

A guide for temperature ranges based on web speed and layer thickness for vinyl is given below in Table II. It should be remembered, however, that the ability of a surface to absorb heat from IR energy is dependent, among other things, on the color of that surface. Thus, the exact temperature within the preferred range will depend on the predominate color of the sheet being embossed. Therefore, these conditions are starting conditions only, and fine tuning adjustments can be made as needed to achieve the product appearance specified by the "standard sample". In fact, in some instances, it may be necessary to operate outside the preferred ranges discussed above to achieve the product appearance specified by the "standard sample".

TABLE II

clear vinyl caliper	web speed (ft./min.)	temperature range °C
.019"	48	155-160
.014"	60	150-155
.012"	70	145-150

Once the wear layer is mechanically embossed, a top coat, also known as a wear layer top coat, is applied to the top and adhered to the embossed wear layer. The top coat can be composed of any suitable material known in the art for this purpose. Preferably, the top coat is a urethane top coat. Once the top coat is applied, the overall surface covering containing all of the layers is cured. Preferably, the top coat has a thickness of from about 0.5 mil to about 2.0 mils, more preferably, from about 0.9 mil to about 1.3 mils.

Optionally, besides the layers discussed above, one or more additional layers can be present, such as the layers described in U.S. Patent No. 5,458,953, incorporated in its entirety by reference herein. Such additional layers include strengthening layers, additional foamable layers, and a wear layer base coat. The composition of these layers and their locations are described in U.S. Patent No. 5,458,953 and can be used in the surface covering of the present invention.

As indicated earlier, the present invention also relates to a surface covering as seen in the photograph of FIG. 3. This surface covering has a backing layer A, a foam layer C and D applied on top and adhered or attached to

the backing layer. A design layer B having a design is printed on the foam layer. At least a portion of the design layer includes a chemically embossed pattern. Preferably, this chemically embossed pattern is in the shape and form of joint or grout lines as previously described. A wear layer is applied on top of the design layer and this wear layer is mechanically embossed with a surface texture. The foam layer C and D may or may not be mechanically embossed. The surface texture is preferably the texture of wood, stone, marble, granite, or brick. Finally, a top coat or wear layer top coat (not shown in FIG. 3) is applied on top of and adhered to the embossed wear layer. The details of each of these components is described above.

As also indicated, additional optional layers such as those described in U.S. Patent No. 5,458,953 can be incorporated into this surface covering. Such additional optional layers include a strengthening layer, a wear layer base coat, and/or additional foam layers.

The present invention will be further clarified by the following examples, which are intended to be purely exemplary of the present invention.

Example 1

A cushioned vinyl floor covering having a backing, a foam layer with a chemically embossed texture in the foam, and a clear vinyl layer was prepared essentially as described in U.S. Patent No. 3,293,108, herein incorporated by reference in its entirety.

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was 0.019 inches (\pm 0.001 inches) thick. Furthermore, the areas that were printed with ink containing a retarder compound, specifically joint or grout lines, had chemical embossing that was a minimum of about .010 inches in depth.

The vinyl flooring material described above was cooled and then mechanically textured in the following manner.

The material was heated by passing it under a gas-fired infrared radiant heater delivering approximately 360 BTU/sq. ft./min.; at a product speed of 37 ft./min. (\pm 2 ft./min.). The heater was positioned between about 3.5 inches and about 6.0 inches above the material surface, depending on the color of the decorative print. The ability of a surface to absorb heat from infrared energy is dependent on such factors as the color of the decorative print. As is well known in the art, the heat delivered by the gas-fired infrared heater described above can be fine-tuned by adjusting the gas-flow controls so that the sheet surface temperature is maintained within the preferred range as given below.

The surface temperature of the material exiting from the heater was approximately between 150°C and 160°C, as measured by a non-contact IR pyrometer held approximately 12-18 inches from the material surface. The back surface of the substrate felt layer was approximately between 80°C and 85°C, as measured by "stick-on" heat tape (for example, "Thermolable," supplied by Paper Thermometer Co., Inc. of Greenfield, NH).

The heated material was then passed through an embossing nip between an engraved steel roll and a rubber back-up roll. The nip was set at 0.050 inches (\pm 0.005 inches) for the material described above. The nip opening was set by

adjustable steel "wedge blocks." Clamping pressure was sufficient so that the nip opening did not vary ("float") while the material was passing through the nip.

The steel roll had an embossing texture engraved onto it by means that are well known in the art. The rubber back-up roll was approximately 90-95 durometer (Shore A). Both rolls were water-cooled such that the surface of the engraved steel roll was approximately 26°C to 38°C, as measured by a contact thermocouple pyrometer.

Following the embossing nip, the material was directed by idler rolls so that it wrapped about one quarter of the engraved roll circumference. The additional contact of material against the water-cooled engraved roll was provided in order to cool the vinyl surface and "set" the embossed texture.

As the final step in preparing a surface covering having a "natural" appearance, the material was coated with a urethane acrylate top coat of the type that was cured by actinic radiation in the UV wavelength region.

The coating was applied to yield a cured thickness approximately between 0.0009 inches and 0.0012 inches. The application was such that the coating followed the embossing texture and did not significantly reduce the embossing depth of the texture. The embossing depth of the mechanical texture in the finished product was between about 0.003 inches and approximately 0.008 inches depending on the specific engraved roll used. However, regardless of the specific engraved roll used, there is no mechanically embossed surface texture in the chemically embossed areas because the minimum chemical embossing

depth of about .010 inches is deeper than the maximum depth of the mechanically embossed surface texture of about .008 inches.

The surface gloss (or "shine") of actinic radiation cured acrylated urethane surface coatings can be varied in a controlled manner to produce the desired visual effect consistent with a "natural" appearance. In one specific example, the appearance of a printed brick design was made more natural by use of a coating with a flat panel 60 degree gloss of about 40 unit.

These actinic radiation cured acrylated urethane coatings are readily available from several commercial suppliers including, but not limited to, Lord Corporation, Erie, Pennsylvania.

Example 2

A cushioned vinyl floor covering having a backing, a foam layer with a chemically embossed texture in the foam, and a clear vinyl layer was prepared as described in Example 1. This vinyl flooring material was cooled and then mechanically textured in the following manner.

The material was heated by passing it under a gas-fired infrared radiant heater delivering approximately 360 BTU/sq. ft./min.; at a product speed of 48ft./min. (\pm 2 ft./min.). The heater was positioned between about 3.5 inches and about 5.0 inches above the material surface, depending on the color of the decorative print. As is well known in the art, the heat delivered by the gas-fired infrared heater described above can be fine-tuned by adjusting the gas-flow

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Following the embossing nip, the material was directed by idler rolls so that it wrapped about one quarter of the engraved roll circumference. The additional contact of material against the water-cooled engraved roll was provided in order to cool the vinyl surface and "set" the embossed texture.

The final step of coating the material with a urethane acrylate top coat was performed as in Example 1 to yield a cured thickness approximately between 0.0009 inches and 0.0012 inches with an embossing depth of the mechanical texture in the finished product being between about 0.003 inches and approximately 0.008 inches depending on the specific engraved roll used.

Other embodiments of the present invention will be apparent to those skilled in the art from consideration of the specification and practice of the invention disclosed herein. It is intended that the specification and examples be considered as exemplary only, with a true scope and spirit of the invention being indicated by the following claims.